

Material	Aluminum	Brass	Stainless Steel	Fused Silica	Invar
thermal expansion ( $10^{-6}$ / K)	25	20	11	4.8	0.6 – 1.3
Sound speed ( $10^3$ m/s)	6.4	3.7	5.8	6.0	

Mirror	Diameter	Thickness	Side 1	Side 2	wedge	Radius of curvature
M1	7.75 mm	4 mm	R > 99.9%, 0° inc	R < 0.2%	< 30 amin	Flat PL/PL
M2	1"	0.25"	R ≥ 99.97%, 0° inc	R < 0.2%	< 30 amin	Flat PL/PL
M3	1"	0.25"	T ~ 1% , 45° inc, P-pol	R < 0.2%	30 amin	Flat PL/PL
M4	1"	0.25"	T ~ 1% , 45° inc, P-pol	R < 0.2%	30 amin	1 m, CC/PL

All mirrors are to be super-polished fused silica. Mirrors M3 and M4 are to be matched in transmission as closely as possible. The main beam is P-polarized (parallel to table, piercing the steering mirrors) everywhere from the Faraday Isolator, through the main IFO, and out to the sensing beamlines (it is S-polarized in the input mode cleaner).

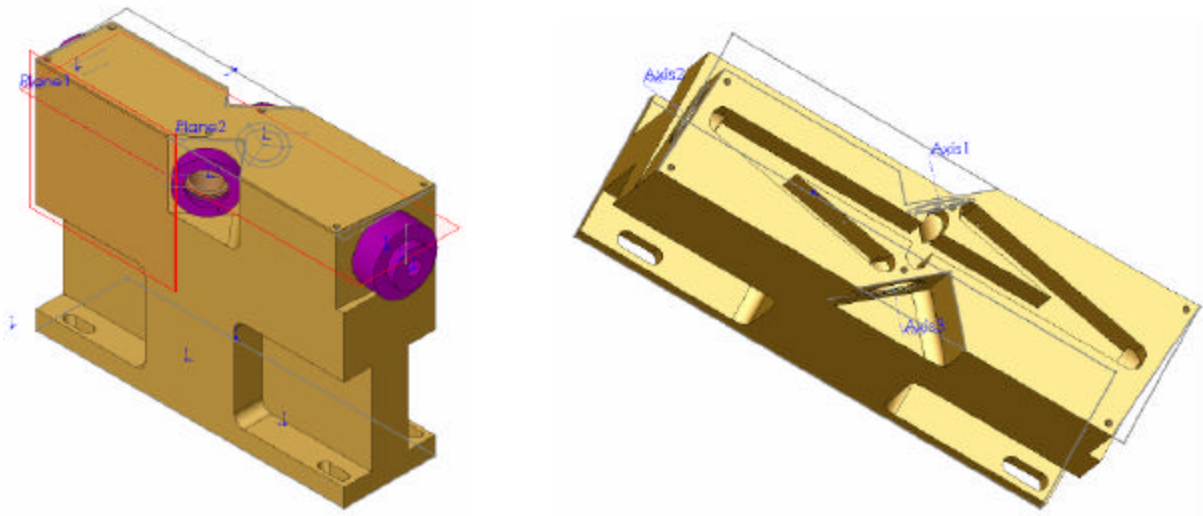


Figure 18: SolidWorks model of a monolithic OMC. Left: Overall view. Right: lifting the lid, here's the optical path for the 4-mirror design.

### 3.3.3 Controlling the OMC

The OMC needs to be locked to the TEM00 carrier light. A length signal can be derived from dithering, PDH reflection, or tilt-locking. The suitably filtered signal can be fed back to the PZT-mounted mirror to acquire and maintain lock.

Dither-locking is relatively simple; we can try it first. We apply a sinusoidal signal to the PZT-mounted mirror to measure its length, and sense that signal in either the reflected or the transmitted light (with a photodiode on a nearby optical table in air). The servo can be implemented with a signal generator / lock-in amplifier, a filtering amplifier, and a PZT driver. Feedback filters can be easily implemented with an analog