

## Cooling of a mirror by radiation pressure

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(March 30, 1999)

We describe an experiment in which a mirror is cooled by the radiation pressure of light. A high-finesse optical cavity with a mirror coated on a mechanical resonator is used as an optomechanical sensor of the Brownian motion of the mirror. A feedback mechanism controls this motion via the radiation pressure of a laser beam reflected on the mirror. We have observed either a cooling or a heating of the mirror, depending on the gain of the feedback loop.

PACS : 05.40.Jc, 04.80.Nn, 42.50.Lc

Thermal noise is a basic limit for many very sensitive optical measurements such as interferometric gravitational-wave detection [1–3]. Brownian motion of suspended mirrors can be decomposed into suspension and internal thermal noises. The latter is due to thermally induced deformations of the mirror surface and constitutes the major limitation of gravitational-wave detectors in the intermediate frequency domain [4,5]. Observation and control of this noise have thus become an important issue in precision measurements [6–9]. In order to reduce thermal noise effects, it is not always possible to lower the temperature and other techniques have been proposed such as a feedback control of a macroscopic oscillator [10].

In this letter we report the first experimental observation of the cooling of a mirror by feedback control via radiation pressure. The basic principle of the experiment is to detect the Brownian motion of the mirror with an optomechanical sensor and then to freeze the motion by applying an electronically controlled radiation pressure on the mirror. Some mechanical effects of light on macroscopic objects have already been observed, such as the dissipative effects of electromagnetic radiation [11], the optical bistability and mirror confinement in a cavity induced by radiation pressure [12,13], or the regulation of the mechanical response of a microcantilever by feedback via the photothermal force [14]. In our experiment the radiation pressure is driven by the feedback loop in such a way that a viscous force is applied to the mirror. It thus plays a role somewhat similar to the one in optical molasses for atoms.

The cooling mechanism can be understood from the experimental setup shown in figure 1. The mirror is used as the rear mirror of a single-ended Fabry-Perot cavity. The phase of the field reflected by the cavity is very sensitive to changes in the cavity length [15–17]. For a resonant cavity, a displacement  $\delta x$  of the rear mirror induces a phase shift  $\delta\varphi_{out}$  of the reflected field on the order of

$$\delta\varphi_{out} \approx \delta\varphi_{in} + \frac{8\mathcal{F}}{\lambda}\delta x, \quad (1)$$

where  $\delta\varphi_{in}$  is the quantum noise of the phase of the incident beam,  $\mathcal{F}$  is the cavity finesse and  $\lambda$  is the optical wavelength. The Brownian motion of the mirror can be detected by measuring the phase of the reflected field, provided that the cavity finesse is high enough [17].

To cool the mirror we use an auxiliary beam derived from the laser and reflected from the back on the mirror. This beam is intensity-modulated by an acousto-optic modulator driven by the feedback loop so that a modulated radiation pressure is applied to the mirror. The resulting motion can be described by its Fourier transform  $\delta x[\Omega]$  at frequency  $\Omega$  which is proportional to the applied forces

$$\delta x[\Omega] = \chi[\Omega] (F_T[\Omega] + F_{rad}[\Omega]), \quad (2)$$

where  $\chi[\Omega]$  is the mechanical susceptibility of the mirror. If we assume that the mechanical response is harmonic, this susceptibility has a lorentzian shape

$$\chi[\Omega] = \frac{1}{M(\Omega_M^2 - \Omega^2 - i\Gamma\Omega)}, \quad (3)$$

characterized by a mass  $M$ , a resonance frequency  $\Omega_M$  and a damping  $\Gamma$  related to the quality factor  $Q$  of the mechanical resonance by  $\Gamma = \Omega_M/Q$ .

The first force  $F_T$  in eq. (2) is a Langevin force responsible for the Brownian motion of the mirror. At thermal equilibrium its spectrum  $S_{F_T}[\Omega]$  is related to the mechanical susceptibility by the fluctuation-dissipation theorem

$$S_{F_T}[\Omega] = -\frac{2k_B T}{\Omega} \text{Im} \left( \frac{1}{\chi[\Omega]} \right) = 2M\Gamma k_B T, \quad (4)$$

where  $T$  is the temperature. The resulting thermal noise spectrum  $S_x^T[\Omega]$  of the mirror motion has a lorentzian shape centered at frequency  $\Omega_M$  and of width  $\Gamma$ .

The second force  $F_{rad}$  in eq. (2) is the radiation pressure exerted by the auxiliary laser beam and modulated

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by the feedback loop. Neglecting the quantum noise  $\delta\varphi_{in}$  in the control signal  $\delta\varphi_{out}$  (eq. 1), this force is proportional to the displacement  $\delta x$  of the mirror. We choose the feedback gain in such a way that the radiation pressure is proportional to the speed  $v = i\Omega\delta x$  of the mirror

$$F_{rad}[\Omega] = iM\Omega g\delta x[\Omega], \quad (5)$$

where  $g$  is related to the electronic gain. The radiation pressure exerted by the auxiliary laser beam thus corresponds to an additional viscous force for the mirror. The resulting motion is given by

$$\delta x[\Omega] = \frac{1}{M[\Omega_M^2 - \Omega^2 - i(\Gamma + g)\Omega]} F_T[\Omega]. \quad (6)$$

This equation is similar to the one obtained without feedback (eq. 2 with  $F_{rad} = 0$ ) except that the radiation pressure changes the damping without adding any fluctuations. The noise spectrum  $S_x^{fb}[\Omega]$  of the mirror motion still has a lorentzian shape but with a different width  $\Gamma_{fb} = \Gamma + g$  and a different height. The variation of height can be characterized by the amplitude noise reduction  $\mathcal{R}$  at resonance frequency

$$\mathcal{R} = \sqrt{\frac{S_x^T[\Omega_M]}{S_x^{fb}[\Omega_M]}} = \frac{\Gamma_{fb}}{\Gamma} = \frac{\Gamma + g}{\Gamma}. \quad (7)$$

The resulting motion is then equivalent to a thermal equilibrium at a different temperature  $T_{fb}$  given by

$$\frac{T_{fb}}{T} = \frac{\Gamma}{\Gamma_{fb}} = \frac{\Gamma}{\Gamma + g}. \quad (8)$$

One can either reduce or increase this effective temperature, depending on the sign of the gain  $g$ .

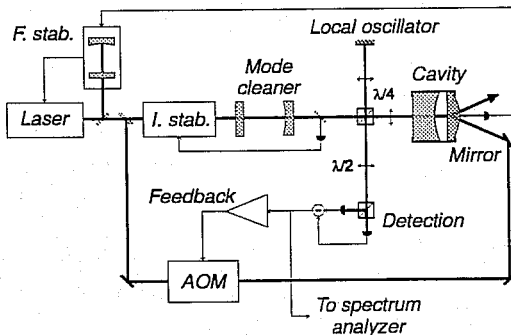


FIG. 1. Experimental setup. The Brownian motion of the mirror is detected with a high-finesse cavity. A light beam provided by a frequency (F. stab.) and intensity (I. stab.) stabilized titane-sapphire laser is sent into the cavity and the phase of the reflected field is measured by homodyne detection. This signal is fed back to the mirror via the radiation pressure exerted by a beam with modulated intensity (AOM)

The model presented here is of course oversimplified. In particular the mirror motion depends on many internal acoustic modes and a description as a single harmonic oscillator may not be appropriate. We have also

neglected the quantum noise  $\delta\varphi_{in}$  in the feedback loop which would induce a lower limit for the effective temperature. This simplified model is however satisfactory to interpret the main features of our current experimental results. In particular we focus in the following on the fundamental acoustic mode of the mirror which has a harmonic response.

We now describe in detail our experiment. The mirror is coated on the plane side of a small plano-convex mechanical resonator made of silica (figure 1). The coating has been made at the *Institut de Physique Nucléaire de Lyon* on a 1.5-mm thick substrate with a diameter of 14 mm and a curvature radius of the convex side of 100 mm. Internal acoustic modes correspond to gaussian modes confined around the central axis of the resonator [18–20]. The fundamental mode studied in this paper is a compression mode with a waist equal to 3.4 mm, a resonance frequency close to 2 MHz and an effective mass of 30 mg [17,20].

The front mirror of the high-finesse cavity has a curvature radius of 1 meter and a typical transmission of 50 ppm (*Newport high-finesse SuperMirror*). This mirror is held at a fixed distance of 1 mm from the back mirror by a rigid cylinder. We have measured the following parameters of the cavity : free spectral range = 141 GHz, cavity bandwidth = 1.9 MHz, beam waist = 90  $\mu\text{m}$ . These values correspond to a finesse  $\mathcal{F}$  of 37000.

The light entering the cavity is provided by a titane-sapphire laser working at 810 nm and frequency-locked to a stable external cavity. The frequency is also locked to a resonance of the high-finesse cavity by monitoring the residual light transmitted by the rear mirror via a control of the external cavity length. The laser intensity is actively stabilized and a mode cleaner reduces the astigmatism of the beam. The light power incident on the cavity is equal to 100  $\mu\text{W}$  with a mode matching of 98%.

The phase of the field reflected by the high-finesse cavity is measured by homodyne detection. The reflected field is mixed on two photodiodes with a 10-mW local oscillator derived from the incident beam. A servoloop monitors the length of the local oscillator arm so that the reflected field is in quadrature with the local oscillator. The difference between the two photocurrents is then proportional to the phase fluctuations  $\delta\varphi_{out}$  of the reflected field. This signal is sent both to the feedback loop and to a spectrum analyzer.

The feedback loop consists of an amplifier with variable gain and phase which drives the acousto-optic modulator. The 500-mW auxiliary beam is uncoupled from the high-finesse cavity by a frequency shift of the acousto-optic modulator (200 MHz) and by a tilt angle of 10° with respect to the cavity axis. We have checked that this beam has no spurious effect on the homodyne detection.

A band-pass filter centered at the fundamental resonance frequency of the mirror is also inserted in the feedback loop to reduce its saturation. For large gains, the

radiation pressure  $F_{rad}$  can become of the same order as the Langevin force  $F_T$  and must be restricted in frequency in order to get a finite variance. The electronic filter has a quality factor of 200 and limits the efficiency of the feedback loop to a bandwidth of 9 kHz around the fundamental resonance frequency.

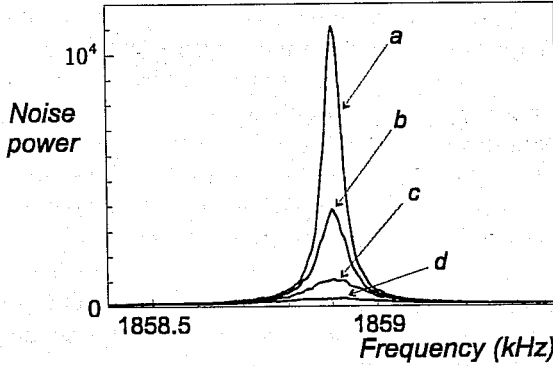


FIG. 2. Phase noise spectrum of the reflected field normalized to the shot-noise level for a frequency span of 1 kHz around the fundamental resonance frequency of the mirror. The peak reflects the Brownian motion of the mirror without feedback (a) and with feedback for increasing gains (b to d)

Figure 2 shows the phase noise spectrum of the reflected field obtained by an average of 1000 scans of the spectrum analyzer with a resolution bandwidth of 10 Hz. Curve (a) is obtained at room temperature without feedback. It reproduces the thermal noise spectrum  $S_x^T$  [ $\Omega$ ] of the mirror which is concentrated around the fundamental resonance frequency (1858.9 kHz) with a width  $\Gamma/2\pi$  of 45 Hz (mechanical quality factor  $Q \simeq 40000$ ). The spectrum is normalized to the shot-noise level and it clearly appears that the thermal noise is much larger than the quantum noise of the measurement [17].

Curves (b) to (d) are obtained with feedback for increasing electronic gains. The phase of the amplifier is adjusted to maximize the correction at resonance. From eqs. (5) and (6) this corresponds to a global imaginary gain for the loop and to a purely viscous radiation pressure force. The control of the mirror motion is clearly visible on those curves. The thermal peak is strongly reduced while its width is increased. The amplitude noise reduction  $\mathcal{R}$  at resonance is larger than 20 for large gains (eq. 7).

The effective temperature  $T_{fb}$  can be deduced from the variance  $\Delta x^2$  of the mirror motion which is equal to the integral of the spectrum  $S_x^{fb}$  [ $\Omega$ ]. From eqs. (4), (6) and (8) one gets the usual relation for a harmonic oscillator at thermal equilibrium

$$\frac{1}{2}M\Omega_M^2\Delta x^2 = \frac{1}{2}k_B T_{fb}. \quad (9)$$

The decrease of the area of the thermal peak observed in figure 2 thus corresponds to a cooling of the mirror.

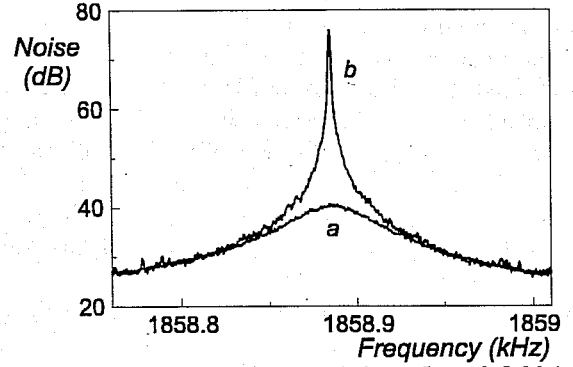


FIG. 3. Phase noise spectrum of the reflected field in dB scale normalized to the shot-noise level for a frequency span of 250 Hz, without feedback (a) and with feedback for a negative gain (b)

Figure 3 shows the effect of feedback for a reverse gain ( $g < 0$ ). Noise spectra are obtained by an average of 500 scans with a resolution bandwidth of 1 Hz. Curve (b) exhibits a strong increase of the thermal peak which now corresponds to a heating of the mirror. The feedback also reduces the damping from  $\Gamma$  to  $\Gamma - |g|$ , thus increasing the quality factor of the resonance. We have obtained a maximum effective quality factor of  $2.2 \times 10^6$  ( $\Gamma_{fb} \simeq \Gamma/50$ ), limited by the saturation of the feedback loop.

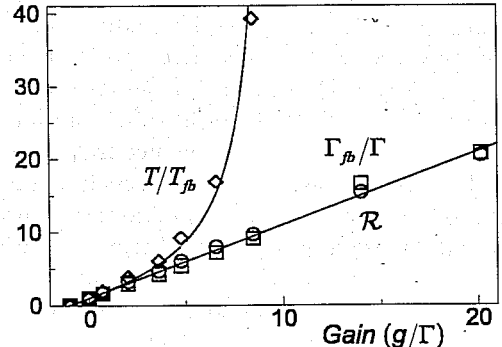


FIG. 4. Variation of the damping  $\Gamma_{fb}/\Gamma$  (squares), of the amplitude noise reduction  $\mathcal{R}$  at resonance (circles) and of the cooling factor  $T/T_{fb}$  (diamonds), as a function of the feedback gain  $g$  normalized to  $\Gamma$ . Solid curves are theoretical results

It is finally instructive to study the efficiency of the cooling or heating mechanism with respect to the gain of the feedback loop. Figure 4 shows the variation of the damping  $\Gamma_{fb}/\Gamma$ , of the amplitude noise reduction  $\mathcal{R}$  at resonance and of the cooling factor  $T/T_{fb}$ , as a function of the feedback gain. These parameters are derived from the experimental spectra by lorentzian fits which give the width and the area of the thermal peak, the latter being related to the effective temperature by eq. (9). To measure the feedback gain, we detect the intensity of the auxiliary beam after reflection on the mirror. The ratio between the modulation spectrum of this intensity at frequency  $\Omega_M$  and the noise spectrum  $S_x^{fb}$  [ $\Omega_M$ ] is proportional to the gain  $g$ . This measurement takes into

account any nonlinearity of the gain due to a possible saturation of the acousto-optic modulator.

As expected from eqs. (6) and (7), the damping and the amplitude noise reduction  $\mathcal{R}$  have a linear dependence with the gain, as well for cooling ( $g > 0$ ) as for heating ( $g < 0$ ). The straight line in figure 4 is in excellent agreement with experimental data and allows to normalize the gain  $g$  to the damping  $\Gamma$ , as this has been done in the figure.

This figure also shows that large cooling factors  $T/T_{fb}$  can be obtained. This cooling factor does not however evolve linearly with the gain as it would be expected from eq. (8). This is due to the presence of a background thermal noise visible in figure 2. This noise is related to all other acoustic modes of the mirror and to the thermal noise of the coupling mirror of the cavity. The feedback loop has not the same effect on this noise and on the fundamental thermal peak. The solid curve in figure 4 corresponds to a theoretical model in which the background noise is assumed to be unchanged by the feedback. As a consequence, only the fundamental mode is cooled at a temperature  $T_{fb}$  whereas all other modes stay in thermal equilibrium at the initial temperature  $T$ . The resulting cooling factor  $T/T_{fb}$  is in excellent agreement with experimental data.

In conclusion, we have observed a cooling of the fundamental acoustic mode of a mirror. The radiation pressure exerted by the feedback loop corresponds to a viscous force which increases the damping of the mirror without adding thermal fluctuations. The Brownian motion is reduced around the fundamental resonance frequency by a factor 20. For large gains, the thermal peak of the fundamental mode becomes of the same order as the background thermal noise and no global thermal equilibrium is reached. As far as an effective temperature can be defined for the fundamental mode, we have obtained a reduction of this temperature by a factor 40.

We have also observed a heating of the mirror for reverse feedback gains. The thermal peak is then sharpened and we have obtained an effective quality factor 50 times larger than the one without feedback.

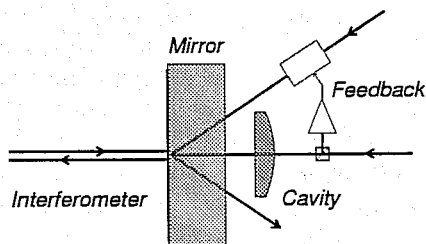


FIG. 5. Application of the cooling mechanism to reduce the thermal noise in a gravitational-wave interferometer

The cooling mechanism demonstrated in this paper may be useful to increase the sensitivity of gravitational-wave interferometers. The main difficulty is to freeze the

thermal noise without changing the effect of the signal. We propose in figure 5 a possible scheme to control the thermal noise of one mirror of the interferometer. A cavity performs a local measurement of the mirror motion which is fed back to the mirror via the radiation pressure of a laser beam. The coupling mirror of the cavity is a small plano-convex mirror with a high mechanical resonance frequency and a low background thermal noise at low frequency. As a consequence the cavity measures the thermal noise of the mirror of the interferometer. For a short cavity, this measurement is not sensitive to a gravitational wave and the cooling reduces the thermal noise without changing the response of the interferometer. To increase the sensitivity of the interferometer at the gravitational-wave frequencies, it is necessary to control the background thermal noise at low frequency instead of controlling the thermal peak at resonance. The principle of the cooling mechanism is however the same as the one demonstrated in this paper as far as the applied radiation pressure can compensate the Langevin force associated with thermal fluctuations.

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